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SOLAR/1087-79/01

Monthly Performance Report

ORTIZ & REILL DEVELOPERS, INC. HOUSE LOT 8

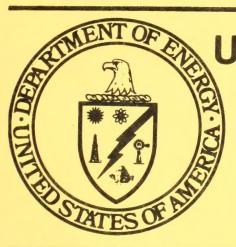
JANUARY 1979





National Solar Heating and Cooling Demonstration Program

National Solar Data Program



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MONTHLY PERFORMANCE REPORT

ORTIZ & REILL DEVELOPERS, INC. HOUSE LOT 8

JANUARY 1979

I. SYSTEM DESCRIPTION

The Ortiz & Reill Developers, Inc., House Lot 8, is one of two instrumented single-family residences in Escondido, California. The home has approximately 1536 square feet of conditioned space. Solar energy is used for domestic-hotwater (DHW) heating and space heating. The solar energy system has an array of flat-plate collectors with a gross area of 192 square feet. The array faces 29 degrees east of south at an angle of 45 degrees to the horizontal. Water is the transfer medium that delivers solar energy from the collector array to storage and to the space heating and hot water loads. Solar energy is stored in a 750-gallon tank located in the ground floor utility room. Heated city water is stored in a 66-gallon DHW tank. When solar energy is insufficient to satisfy the space heating load, a gas furnace provides auxiliary energy for the space heating system. Similarly, an electrical heating element in the DHW tank provides auxiliary energy for DHW heating. Energy from an hydronic fireplace radiates directly into the living space and supplements solar modes 1 and 2. The fireplace-to-storage mode activates if the fireplace is being used, the temperature difference between its water plenum and storage output is more than 9°F, and there is no demand for space heating. During operation, water is circulated from storage through the fireplace heat exchanger. The system, shown schematically in Figure 1, has four modes of solar operation.

Mode 1 - Collector-to-Storage: This mode activates when the temperature at the outlet of the collector array exceeds the temperature at the bottom of the storage tank by more than 9°F. Water is circulated from the tank through the collectors until the temperature difference is less than 3°F.

Mode 2 - Storage-to-Space Heating: This mode activates when the manually preset thermostat located in the heated space indicates a demand for space heating. Heated water is circulated from storage through a heat exchanger in the air-handling unit and returned to storage. If the demand cannot be satisfied by energy from storage, the gas furnace is activated to provide auxiliary heat. The fireplace can also add energy to the water circulating from storage before it enters the air-handling unit. If the fireplace is being used and the temperature difference between its water plenum and storage output is more than 9°F, valve D400 is activated and energy is added to the water from the fireplace heat exchanger.

Mode 3 - Storage-to-DHW: This mode activates when there is a temperature difference exceeding a pre-set differential between storage and the DHW tank and there is no demand for space heating. Incoming city water enters the DHW tank, where it is heated by water circulating from storage through a heat exchanger in the tank.

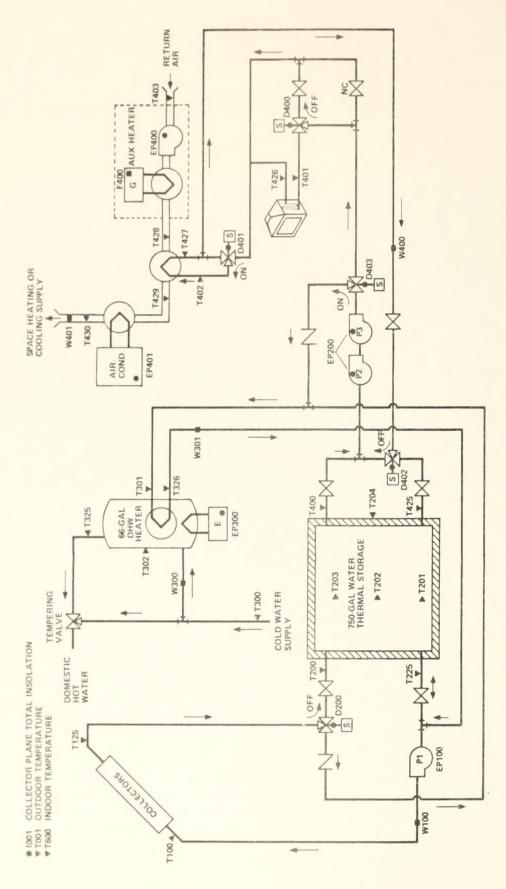


Figure 1. ORTIZ AND REILL DEVELOPERS, INC., LOT NO. 8 SOLAR ENERGY SYSTEM SCHEMATIC

Mode 4 - Collector-to-DHW: This mode activates when the temperature in the DHW tank falls below $140^{\circ}F$ and the collector output temperature exceeds the DHW tank temperature. Water circulates through the heat exchanger in the DHW tank and returns to the collectors.

II. PERFORMANCE EVALUATION

INTRODUCTION

The site was occupied in January and the solar energy system operated continuously during the month. Solar energy satisfied 51 percent of the DHW requirements and 26 percent of the space heating requirements. The solar energy system provided electrical energy savings of 0.11 million Btu and a fossil fuel energy savings of 0.56 million Btu.

WEATHER CONDITIONS

During the month, total incident solar energy on the collector array was 6.4 million Btu for a daily average of 1077 Btu per square foot. This was below the estimated average daily solar radiation for this geographical area during January of 1504 Btu per square foot for a plane facing 29 degrees east of south with a tilt of 45 degrees to the horizontal. The average ambient temperature during January was 51°F as compared with the long-term average for January of 55°F. The number of heating degree-days for the month (based on a 65°F reference) was 428, as compared with the long-term average of 314. The number of cooling degree-days was zero, as compared with the average of 10.

THERMAL PERFORMANCE

Collector - The total incident solar radiation on the collector array for the month of January was 6.4 million Btu. During the period the collector loop was operating the total insolation amounted to 5.1 million Btu. The total collected solar energy for the month of January was 1.7 million Btu, resulting in a collector array efficiency of 26 percent, based on total incident insolation. Solar energy delivered from the collector array to storage was 0.80 million Btu, while solar energy delivered from the collector array directly to the loads amounted to 0.30 million Btu. Energy loss during transfer from the collector array to storage and loads was 0.60 million Btu. This loss represented 35 percent of the energy collected. Operating energy required by the collector loop was 0.064 million Btu.

Storage - Solar energy delivered to storage was 0.80 million Btu and auxiliary energy contribution to storage was 0.18 million Btu. There were 0.46 million Btu delivered from storage to the DHW and space heating subsystems. Energy loss from storage was 0.54 million Btu and represented 55 percent of the energy delivered to storage. The storage efficiency was 45 percent: This is calculated as the ratio of the sum of the energy removed from storage and the change in stored energy, to the energy delivered to storage. The average storage temperature for the month was 92°F.

DHW Load - The DHW subsystem consumed 0.42 million Btu of solar energy and 0.49 million Btu of auxiliary electrical energy to satisfy a hot water load of 0.96 million Btu. The solar fraction of this load was 51 percent. The DHW subsystem consumed a total of 0.22 million Btu of operating energy, resulting in an electrical energy savings of 0.20 million Btu. The amount of solar energy used by the DHW subsystem is believed to be slightly greater than indicated. This discrepancy is attributed to problems in data resolution and to temperature sensor resolution limitations. The DHW solar fraction and energy savings are believed to be slightly greater than indicated for the same reasons. A daily average of 54 gallons of DHW was consumed at an average temperature of 132°F delivered from the tank.

Space Heating Load - The space heating subsystem consumed 0.34 million Btu of solar energy and 1.0 million Btu of auxiliary thermal energy (equivalent to 1.7 million Btu of auxiliary fossil fuel energy) to satisfy a space heating load of 1.3 million Btu. The solar fraction of this load was 26 percent. The space heating subsystem consumed a total of 0.23 million Btu of operating energy, resulting in an electrical energy expense of 0.027 million Btu and a fossil fuel energy savings of 0.56 million Btu.

OBSERVATIONS

In satisfying 34 percent of the combined DHW and space heating demand a total of 1.1 million Btu was lost from the system. The system loss represented 65 percent of the energy collected.

For several hours during the month the control system allowed simultaneous operation in the conventional space heating mode and the storage-to-space heating mode. This resulted in an small amount of fossil fuel energy being transferred to storage from the space heating subsystem.

The fireplace operated intermittently during the month in the fireplace-tostorage mode and contributed approximately 0.17 million Btu to storage.

Fireplace contribution was insignificant during January. There was erratic operation in the fireplace and storage-to-space heating mode for only 20 minutes during the month.

ENERGY SAVINGS

The solar energy system provided a net electrical energy savings of 0.11 million Btu and a fossil fuel energy savings of 0.56 million Btu. The DHW subsystem provided an electrical energy savings of 0.20 million Btu, while the space heating subsystem incurred an electrical energy expense of 0.027 million Btu and fossil fuel energy savings of 0.56 million Btu.

III. ACTION STATUS

The grantee is investigating and implementing control system improvements. No additional action is planned at this time.

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